

## Chapter 3: Work-Energy Theorem

# Newton's Law of Motion

- First we define the momentum ( $\mathbf{p}$ ) of a particle (or a more complicated system) as

$$\mathbf{p} = m\mathbf{v},$$

where  $m$  is the mass of the system, and  $\mathbf{v}$  is its velocity.

- Newtons' second law of motion states that force  $\mathbf{F}$  acting on a system is equal to its rate of change of momentum

$$\mathbf{F} = \frac{d\mathbf{p}}{dt}.$$

- This is the most general definition of Newton's second law of motion and is applicable also to those systems, such as a rocket, whose mass  $m$  is not constant.
- However, for a system whose mass does not change with time, we have its more familiar form

$$\mathbf{F} = \frac{d(m\mathbf{v})}{dt} = m\frac{d\mathbf{v}}{dt} = m\mathbf{a}.$$

- Next, we explore some consequences of Newton's second law.

# Work and Energy

- Consider a 1D system confined to move in  $x$  direction
- Let the force acting on a system of mass  $m$ , be  $F(x)$
- Thus the force can depend on the position
- Then the work done  $dW$  in moving the particle by an infinitesimal amount  $dx$  is given by

$$dW = F(x)dx$$

- Thus, the work done  $W_{ab}$  in moving the particle from position  $x = a$  to  $x = b$ , will be the integral of the expression above

$$W_{ab} = \int_a^b F(x)dx$$

# Work-Energy relationship

- Let us manipulate this expression

$$\begin{aligned}W_{ab} &= \int_a^b F(x) dx \\&= \int_a^b m a dx \\&= m \int_a^b \frac{dv}{dt} dx.\end{aligned}$$

- But, we can write

$$dx = \frac{dx}{dt} dt = v dt.$$

- Substituting it above, we have

$$\begin{aligned}W_{ab} &= m \int_a^b \frac{dv}{dt} v dt = m \int_a^b \frac{1}{2} \frac{dv^2}{dt} dt = \int_a^b \frac{d}{dt} \left( \frac{1}{2} m v^2 \right) dt \\ \implies W_{ab} &= \frac{1}{2} m v_b^2 - \frac{1}{2} m v_a^2\end{aligned}$$

# Work-Energy Theorem

- Thus, we have shown in 1D that work done on a particle in taking it from point A to B, is nothing but change in its kinetic energy during the journey
- This is nothing but the statement of work-energy theorem in 1D
- But most forces are three dimensional in nature, as are most of the displacements
- For a 3D case, the force  $\mathbf{F}$ , at position  $\mathbf{r} = x\hat{\mathbf{i}} + y\hat{\mathbf{j}} + z\hat{\mathbf{k}}$ , can be written in terms of Cartesian components as

$$\mathbf{F}(\mathbf{r}) = \mathbf{F}(x, y, z) = F_x(x, y, z)\hat{\mathbf{i}} + F_y(x, y, z)\hat{\mathbf{j}} + F_z(x, y, z)\hat{\mathbf{k}}$$

- Note that each component of force is a function of all the three Cartesian coordinates
- A position dependent vector quantity such as  $\mathbf{F}(\mathbf{r})$ , is called a vector field.

# Work-Energy Theorem in 3D

- Suppose this force displaces a particle of mass  $m$  by an infinitesimal vector  $d\mathbf{r} = dx\hat{\mathbf{i}} + dy\hat{\mathbf{j}} + dz\hat{\mathbf{k}}$ , then the total work done will be

$$dW = F_x dx + F_y dy + F_z dz = \mathbf{F} \cdot d\mathbf{r}$$

- Obviously, work done in displacing the particle by a finite amount, starting from  $\mathbf{r} = \mathbf{r}_a$  to  $\mathbf{r} = \mathbf{r}_b$ , will be

$$W_{ab} = \int_{\mathbf{r}_a}^{\mathbf{r}_b} \mathbf{F} \cdot d\mathbf{r}.$$

Such three dimensional integrals are called line integrals, which need to be evaluated along a path.

- Similar to the 1D case, we have

$$d\mathbf{r} = \frac{d\mathbf{r}}{dt} dt = \mathbf{v} dt$$

# Work-Energy Theorem 3D...

- Then

$$\begin{aligned}W_{ab} &= \int_{\mathbf{r}_a}^{\mathbf{r}_b} \mathbf{F} \cdot d\mathbf{r} = \int_{\mathbf{r}_a}^{\mathbf{r}_b} m \frac{d\mathbf{v}}{dt} \cdot \mathbf{v} dt = \int_{\mathbf{r}_a}^{\mathbf{r}_b} \frac{d}{dt} \left( \frac{1}{2} m \mathbf{v} \cdot \mathbf{v} \right) dt \\&= \int_{\mathbf{r}_a}^{\mathbf{r}_b} \frac{d}{dt} \left( \frac{1}{2} m v^2 \right) dt\end{aligned}$$

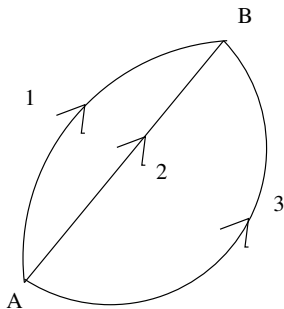
- Finally

$$W_{ab} = \int_{\mathbf{r}_a}^{\mathbf{r}_b} \mathbf{F} \cdot d\mathbf{r} = \frac{1}{2} m v_b^2 - \frac{1}{2} m v_a^2.$$

- Thus the form of Work-Energy theorem in 3D is similar to that in 1D

# Line Integrals

- Because work done is expressed in terms of a line integral ( $W_{ab} = \int_{\mathbf{r}_a}^{\mathbf{r}_b} \mathbf{F} \cdot d\mathbf{r}$ ), it will, in principle, depend on the path connecting points A and B.
- For example, for the three paths shown below, the line integral, in general, will have three different values



- Do we have forces  $\mathbf{F}(\mathbf{r})$  for which this line integral is path independent?

# Conservative Forces

- Most fundamental forces in nature satisfy this property
- Examples: gravitational force, electrostatic force
- For such forces work done will not depend on the path of displacement
- Rather it will depend only on the positions of the end points (A and B in this case) of the path
- Such forces are called “Conservative Forces”

# Potential Energy

- Thus, for conservative forces, a mathematical function  $V(\mathbf{r})$  exists such that

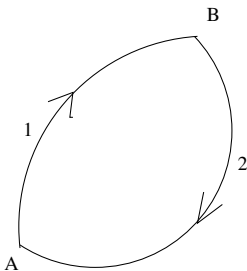
$$W_{ab} = \int_{\mathbf{r}_a}^{\mathbf{r}_b} \mathbf{F} \cdot d\mathbf{r} = -(V(\mathbf{r}_b) - V(\mathbf{r}_a))$$

Above negative sign on the RHS is chosen as a matter of convention

- If such a function  $V(\mathbf{r})$  did not exist, line integral will always depend on the path connecting A and B
- Thus  $V(\mathbf{r})$  guarantees that the work done depends only on the endpoints of the path, and not the path itself
- The function  $V(\mathbf{r})$  has dimensions of energy, and is called the potential energy.  $V(\mathbf{r})$  is a scalar field, unlike  $\mathbf{F}(\mathbf{r})$ , which is a vector field.

# Potential energy: properties

- It is easier to deal with scalars rather than vectors, because one doesn't have to worry about a direction.
- For conservative forces, work done along a closed path is zero
- Consider the closed path shown below



- Along the closed path shown above

$$\begin{aligned}\oint \mathbf{F} \cdot d\mathbf{r} &= \int_{\mathbf{r}_a}^{\mathbf{r}_b} \mathbf{F} \cdot d\mathbf{r} + \int_{\mathbf{r}_b}^{\mathbf{r}_a} \mathbf{F} \cdot d\mathbf{r} \\ &= -(V(\mathbf{r}_b) - V(\mathbf{r}_a)) - (V(\mathbf{r}_a) - V(\mathbf{r}_b)) \\ &= 0\end{aligned}$$

# Conservation of Energy

- A consequence of work-energy theorem for conservative forces is that sum of kinetic and potential energies of a system is conserved
- For a conservative force we have

$$W_{ab} = \int_{\mathbf{r}_a}^{\mathbf{r}_b} \mathbf{F} \cdot d\mathbf{r} = \frac{1}{2}mv_b^2 - \frac{1}{2}mv_a^2 = V(\mathbf{r}_a) - V(\mathbf{r}_b)$$
$$\implies \frac{1}{2}mv_a^2 + V(\mathbf{r}_a) = \frac{1}{2}mv_b^2 + V(\mathbf{r}_b)$$

which is nothing but conservation of total energy (kinetic + potential)

- That is the reason behind the name “conservative force”.

# Potential energy at a point

- So far we have computed only the potential energy difference between two points (A and B, say)
- How do we define the potential energy  $V(\mathbf{r})$ , at a given point  $\mathbf{r}$  in space?
- It is defined with respect to a reference point  $\mathbf{r}_O$ , which is normally taken to be infinity
- It is defined as the work done against the force  $\mathbf{F}(\mathbf{r})$ , in bringing the particle from the reference point O to point  $\mathbf{r}$

$$V(\mathbf{r}) = - \int_{\mathbf{r}_O}^{\mathbf{r}} \mathbf{F}(\mathbf{r}) \cdot d\mathbf{r}$$

# Relation between force and potential energy

- Consider a 1D conservative force, so that

$$V(b) - V(a) = - \int_a^b F(x) dx.$$

- Let points  $x = a$  and  $x = b$  be infinitesimally close to each other, i.e.,  $a = x$  and  $b = x + \Delta x$ , with  $\Delta x$  small

$$V(x + \Delta x) - V(x) = - \int_x^{x+\Delta x} F(x') dx'.$$

- We define  $\Delta V(x) = V(x + \Delta x) - V(x)$ , and for small  $\Delta x$ , we have

$$\int_x^{x+\Delta x} F(x') dx' \approx F(x) \Delta x + \dots$$

- Substituting it above, we obtain

$$\Delta V \approx -F(x) \Delta x$$

$$F(x) \approx -\frac{\Delta V}{\Delta x}.$$

# Force and Potential Energy....

- In the limit  $\Delta x \rightarrow 0$ , we get

$$F(x) = -\frac{dV}{dx}$$

- This is the required relationship between  $F$  and  $V$  in 1D.
- How to generalize it to 3D?

# Force and Potential Energy: Connection in 3D

- In 3D, both  $\mathbf{F}(\mathbf{r})$  and  $V(\mathbf{r})$  are functions of all three Cartesian coordinates  $x$ ,  $y$ , and  $z$ .
- So, we have to be careful with our mathematics
- We know

$$V(\mathbf{r}_b) - V(\mathbf{r}_a) = - \int_{\mathbf{r}_a}^{\mathbf{r}_b} \mathbf{F} \cdot d\mathbf{r}.$$

- As before, we choose  $\mathbf{r}_a = \mathbf{r}$  and  $\mathbf{r}_b = \mathbf{r} + \Delta\mathbf{r}$ , to obtain

$$V(\mathbf{r} + \Delta\mathbf{r}) - V(\mathbf{r}) = - \int_{\mathbf{r}}^{\mathbf{r} + \Delta\mathbf{r}} \mathbf{F} \cdot d\mathbf{r}'.$$

- Because  $\Delta\mathbf{r} = \Delta x \hat{\mathbf{i}} + \Delta y \hat{\mathbf{j}} + \Delta z \hat{\mathbf{k}}$  is an infinitesimal displacement vector in 3D, so

$$- \int_{\mathbf{r}}^{\mathbf{r} + \Delta\mathbf{r}} \mathbf{F} \cdot d\mathbf{r}' \approx -\mathbf{F}(\mathbf{r}) \cdot \Delta\mathbf{r} = -F_x \Delta x - F_y \Delta y - F_z \Delta z$$

# Force and Potential Energy in 3D....

- To compute  $V(\mathbf{r} + \Delta\mathbf{r}) - V(\mathbf{r})$ , we use Taylor's expansion for multiple variables

$$\begin{aligned} V(\mathbf{r} + \Delta\mathbf{r}) &= V(x + \Delta x, y + \Delta y, z + \Delta z) \\ &= V(x, y, z) + \frac{\partial V}{\partial x} \Delta x + \frac{\partial V}{\partial y} \Delta y + \frac{\partial V}{\partial z} \Delta z + O(dr^2) \\ &= V(\mathbf{r}) + \nabla V \cdot \Delta\mathbf{r} + O(dr^2) \end{aligned}$$

- Symbol  $\nabla V$ , stands for “gradient of  $V$ ”, defined as

$$\nabla V = \frac{\partial V}{\partial x} \hat{\mathbf{i}} + \frac{\partial V}{\partial y} \hat{\mathbf{j}} + \frac{\partial V}{\partial z} \hat{\mathbf{k}}$$

- $\frac{\partial V}{\partial x}$ ,  $\frac{\partial V}{\partial y}$ , and  $\frac{\partial V}{\partial z}$  are called “partial derivatives”, computed by taking the derivative with respect to the given variable (say  $x$ ), treating other two variables (say  $y$  and  $z$ ) as constants.
- Note that gradient operator applies on a scalar field, and the result is a vector field.

- With this

$$V(\mathbf{r} + \Delta\mathbf{r}) - V(\mathbf{r}) = \nabla V \cdot \Delta\mathbf{r} = -\mathbf{F}(\mathbf{r}) \cdot \Delta\mathbf{r}.$$

- Because  $\Delta\mathbf{r}$  is an arbitrary displacement, therefore,

$$\begin{aligned}\nabla V \cdot \Delta\mathbf{r} &= -\mathbf{F}(\mathbf{r}) \cdot \Delta\mathbf{r} \\ \implies \mathbf{F}(\mathbf{r}) &= -\nabla V\end{aligned}$$

- This is a very important result showing that a conservative force can be written as the gradient of corresponding potential energy.
- Before we proceed further, let us have a bit of mathematical exploration

# Calculation of Gradient: Example 1

- First let us compute a few partial derivatives
- Let  $f(x, y, z) = r^2 = x^2 + y^2 + z^2$ , then

$$\frac{\partial f}{\partial x} = 2x$$

$$\frac{\partial f}{\partial y} = 2y$$

$$\frac{\partial f}{\partial z} = 2z$$

- So that

$$\nabla f = 2(x\hat{\mathbf{i}} + y\hat{\mathbf{j}} + z\hat{\mathbf{k}}) = 2\mathbf{r}$$

## Calculation of Gradient: Example 2

- Let  $g(x, y, z) = xyz$ , then

$$\frac{\partial g}{\partial x} = yz$$

$$\frac{\partial g}{\partial y} = xz$$

$$\frac{\partial g}{\partial z} = xy$$

- So that

$$\nabla g = yz\hat{\mathbf{i}} + xz\hat{\mathbf{j}} + xy\hat{\mathbf{k}}$$

# A few suggested exercises

- Compute the gradient of the following scalar functions

$$f(x, y, z) = x^4 + y^4 + z^4$$

$$g(x, y, z) = x^2y^2 + y^2z^2 + z^2x^2$$

$$\Phi(x, y, z) = 3xy^2z^3 + 2xyz + 4x^2y^2$$

- Gradient and other functions can also be computed in other coordinate systems such as plane-polar coordinates

# A bit of vector calculus: Gradient of a Scalar Function

- Consider a scalar function  $T(x, y, z)$
- We want to compute the change in  $T$ , as we move from initial coordinates  $\mathbf{r} \equiv (x, y, z)$  infinitesimally to the new position  $\mathbf{r} + d\mathbf{r} \equiv (x + dx, y + dy, z + dz)$
- Using Taylor expansion (for multi-variables), and retaining terms up to first order

$$T(\mathbf{r} + d\mathbf{r}) = T(\mathbf{r}) + dx \frac{\partial T}{\partial x} + dy \frac{\partial T}{\partial y} + dz \frac{\partial T}{\partial z} + \text{higher order terms}$$

- Or, to the first order terms,

$$T(\mathbf{r} + d\mathbf{r}) = T(\mathbf{r}) + d\mathbf{r} \cdot \nabla T$$

- Where

$$d\mathbf{r} = dx\hat{i} + dy\hat{j} + dz\hat{k}$$
$$\nabla T = \frac{\partial T}{\partial x}\hat{i} + \frac{\partial T}{\partial y}\hat{j} + \frac{\partial T}{\partial z}\hat{k}$$

- Defining  $T(\mathbf{r} + d\mathbf{r}) = T(\mathbf{r}) + dT$ , we conclude

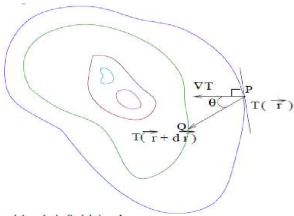
$$dT = d\mathbf{r} \cdot \nabla T,$$

where the vector  $\nabla T$  defined above is called the **gradient** of scalar field  $T$ .

- Thus  $\nabla T$  defines the rate of change of the scalar field with respect to the spatial coordinates, and is itself a vector quantity
- Let us examine  $\nabla T$  a bit more

# Physical Meaning of Gradient

- Let us plot the constant surfaces of a given scalar field  $T$



- As per the figure, we can write the change in the scalar field  $dT$  as

$$dT = \mathbf{dr} \cdot \nabla T = |\mathbf{dr}| |\nabla T| \cos \theta$$

- Let us consider two possibilities:
  - $\mathbf{dr}$  is along a constant  $T$  surface
  - $\mathbf{dr}$  is in an arbitrary direction

## Gradient, physical meaning...

- If  $d\mathbf{r}$  is along a constant  $T$  surface then  $dT = 0$ . This means

$$\begin{aligned} |\mathbf{dr}||\nabla T| \cos \theta &= 0 \\ \implies \cos \theta &= 0 \end{aligned}$$

- Thus the direction of  $\nabla T$  at a given point  $\mathbf{r}$  is always perpendicular to the constant  $T$  surface passing through that point
- Let us consider  $d\mathbf{r}$  to be in an arbitrary direction
- Then from  $dT = |\mathbf{dr}||\nabla T| \cos \theta$ , it is obvious that the magnitude of the maximum possible change in  $T$  is

$$dT_{max} = |\mathbf{dr}||\nabla T|,$$

i.e., when  $\cos \theta = 1$ .

- Thus the direction of  $\nabla T$  is also the direction of maximum change in the scalar function  $T$ .

## Gradient continued...

- Thus, at a given point  $\mathbf{r}$ , if one moves in the direction of  $\nabla T$ , maximum change in  $T$  will take place
- This property of gradient is used in optimization problems involving location of maxima/minima of scalar functions

### Examples:

- 1 Let us consider a scalar function

$$T = r^2 = x^2 + y^2 + z^2$$

It is easy to see that

$$\nabla T = \frac{\partial T}{\partial x} \hat{i} + \frac{\partial T}{\partial y} \hat{j} + \frac{\partial T}{\partial z} \hat{k} = 2x\hat{i} + 2y\hat{j} + 2z\hat{k} = 2\mathbf{r}$$

- 2 Consider  $\Phi(x, y, z) = x^2y + y^2z + z^2x + 2xyz$

# Gradient calculation

Clearly

$$\begin{aligned}\nabla\Phi &= \frac{\partial\Phi}{\partial x}\hat{i} + \frac{\partial\Phi}{\partial y}\hat{j} + \frac{\partial\Phi}{\partial z}\hat{k} \\ &= (2xy + 2yz + z^2)\hat{i} + (2yz + 2xz + x^2)\hat{j} + (2zx + 2xy + y^2)\hat{k}\end{aligned}$$

- Thus, in Cartesian coordinates, the gradient operator can be denoted as

$$\nabla \equiv \frac{\partial}{\partial x}\hat{i} + \frac{\partial}{\partial y}\hat{j} + \frac{\partial}{\partial z}\hat{k}$$

- In curvilinear coordinates the gradient operator has more complicated forms

$$\text{Cylindrical } \nabla \equiv \frac{\partial}{\partial \rho}\hat{\rho} + \frac{\partial}{\rho\partial\theta}\hat{\theta} + \frac{\partial}{\partial z}\hat{k}$$

$$\text{Spherical } \nabla \equiv \frac{\partial}{\partial r}\hat{r} + \frac{\partial}{r\partial\theta}\hat{\theta} + \frac{\partial}{r\sin\theta\partial\phi}\hat{\phi}$$

# Some Properties of Gradient

1

$$\nabla(U + V) = \nabla U + \nabla V$$

2

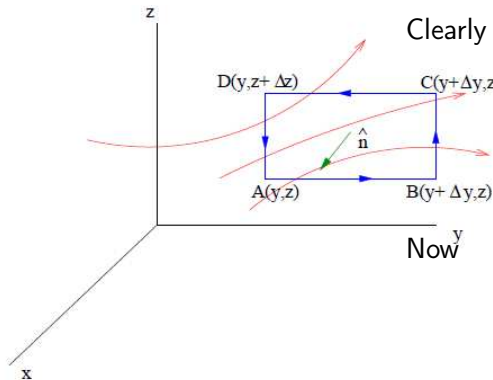
$$\nabla(UV) = U\nabla V + V\nabla U$$

3

$$\nabla(V^n) = nV^{n-1}\nabla V$$

# Curl of a Vector Field

Let us consider a vector field  $\mathbf{F} = F_x \hat{i} + F_y \hat{j} + F_z \hat{k}$ , and evaluate its line integral along a infinitesimal rectangular path shown below



$$\oint \mathbf{F} \cdot d\mathbf{l} = \int_{AB} \mathbf{F} \cdot d\mathbf{l} + \int_{BC} \mathbf{F} \cdot d\mathbf{l} + \int_{CD} \mathbf{F} \cdot d\mathbf{l} + \int_{DA} \mathbf{F} \cdot d\mathbf{l}$$

$$\begin{aligned} \int_{AB} \mathbf{F} \cdot d\mathbf{l} &= \int \mathbf{F} \cdot dy \hat{j} \approx F_y(y, z) \Delta y \\ \int_{BC} \mathbf{F} \cdot d\mathbf{l} &= \int \mathbf{F} \cdot dz \hat{k} \\ &\approx F_z(y + \Delta y, z) \Delta z \end{aligned}$$

## Curl contd....

Using first order Taylor expansion

$$F_z(y + \Delta y, z) = F_z(y, z) + \frac{\partial F_z}{\partial y} \Delta y$$

So that

$$\int_{AB} \mathbf{F} \cdot d\mathbf{l} + \int_{BC} \mathbf{F} \cdot d\mathbf{l} = \left( F_y \Delta y + F_z \Delta z + \frac{\partial F_z}{\partial y} \Delta z \Delta y \right)$$

Similarly one can show (by integrating in AD and DC directions)

$$\int_{CD} \mathbf{F} \cdot d\mathbf{l} + \int_{DA} \mathbf{F} \cdot d\mathbf{l} = - \left( F_y \Delta y + F_z \Delta z + \frac{\partial F_y}{\partial z} \Delta z \Delta y \right)$$

By adding all the contributions we obtain

$$\oint \mathbf{F} \cdot d\mathbf{l} = \left( \frac{\partial F_z}{\partial y} - \frac{\partial F_y}{\partial z} \right) \Delta S_x \quad (1)$$

Where  $\Delta S_x = \Delta y \Delta z$ , is the area of the infinitesimal loop, directed along the  $x$  axis. Let us define a quantity called **curl**, denoted as  $\nabla \times$

$$\nabla \times \mathbf{F} = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ F_x & F_y & F_z \end{vmatrix}.$$

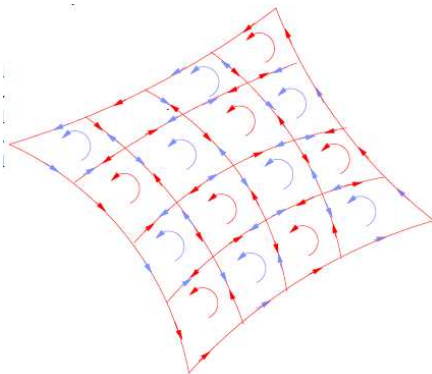
Using this we can cast Eq. 1 as

$$\oint \mathbf{F} \cdot d\mathbf{l} = (\nabla \times \mathbf{F})_x \Delta S_x = (\nabla \times \mathbf{F}) \cdot \Delta \mathbf{S} \quad (2)$$

# Stokes' Theorem

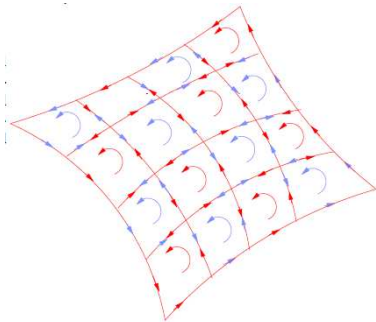
**Stokes' Theorem:** If a vector field  $\mathbf{F}$  is integrated along a closed loop of an arbitrary shape, then the line integral is equal to the surface integral of the curl of  $\mathbf{F}$ , evaluated over the area enclosed by the loop

$$\oint \mathbf{F} \cdot d\mathbf{l} = \int_S (\nabla \times \mathbf{F}) \cdot d\mathbf{S}$$



# Proof of Stokes' Theorem

## Outline of the proof:



We can split the area enclosed by the loop into a large number of infinitesimal loops as shown, for each one of which Eq. 2 will hold. Upon adding the contribution of all such loops, we get the desired result

$$\oint \mathbf{F} \cdot d\mathbf{l} = \int_S (\nabla \times \mathbf{F}) \cdot d\mathbf{S}.$$

Note that in the line integral, the contribution only from the boundary of the loop will survive because the contribution from the internal lines gets canceled from adjacent loops.

**Curl in Cylindrical Coordinates:** For a vector field

$$\mathbf{A} = A_\rho \hat{\rho} + A_\theta \hat{\theta} + A_z \hat{z}$$

$$\begin{aligned}\nabla \times \mathbf{A} = & \left( \frac{1}{\rho} \frac{\partial A_z}{\partial \theta} - \frac{\partial A_\theta}{\partial z} \right) \hat{\rho} \\ & + \left( \frac{\partial A_\rho}{\partial z} - \frac{\partial A_z}{\partial \rho} \right) \hat{\theta} \\ & + \frac{1}{\rho} \left( \frac{\partial (\rho A_\theta)}{\partial \rho} - \frac{\partial A_\rho}{\partial \phi} \right) \hat{z}\end{aligned}$$

# Curl in Spherical Polar Coordinate System

Curl in Spherical Polar Coordinates: For a vector field

$$\mathbf{A} = A_r \hat{\mathbf{r}} + A_\theta \hat{\boldsymbol{\theta}} + A_\phi \hat{\boldsymbol{\phi}}$$

$$\begin{aligned}\nabla \times \mathbf{A} = & \frac{1}{r \sin \theta} \left( \frac{\partial}{\partial \theta} (A_\phi \sin \theta) - \frac{\partial A_\theta}{\partial \phi} \right) \hat{\mathbf{r}} \\ & + \frac{1}{r} \left( \frac{1}{\sin \theta} \frac{\partial A_r}{\partial \phi} - \frac{\partial}{\partial r} (r A_\phi) \right) \hat{\boldsymbol{\theta}} \\ & + \frac{1}{r} \left( \frac{\partial}{\partial r} (r A_\theta) - \frac{\partial A_r}{\partial \theta} \right) \hat{\boldsymbol{\phi}}\end{aligned}$$

# Examples of Calculation of Curl

- ① Calculate the curl of the vector field  $\mathbf{F} = -y\hat{i} + z\hat{j} + x^2\hat{k}$

$$\begin{aligned}\nabla \times \mathbf{F} &= \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ -y & z & x^2 \end{vmatrix} \\ &= -\hat{i} + 2x\hat{j} + \hat{k}\end{aligned}$$

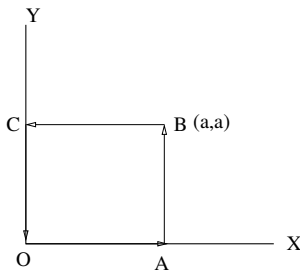
- ② Easy to verify that  $\nabla \times \mathbf{r} = 0$ , where  $\mathbf{r} = x\hat{i} + y\hat{j} + z\hat{k}$ .

# Stokes theorem: An example

- Consider a 2D vector field

$$\mathbf{F} = -y\hat{\mathbf{i}} + x\hat{\mathbf{j}}$$

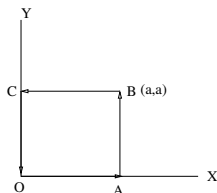
- And a closed loop shaped like a square as shown



- Let us verify Stokes theorem for this case.

$$\oint \mathbf{F} \cdot d\mathbf{l} = \int_S (\nabla \times \mathbf{F}) \cdot d\mathbf{S}.$$

# Stokes theorem, example contd.



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- LHS of Stokes theorem

$$\oint \mathbf{F} \cdot d\mathbf{l} = \int_{OA} \mathbf{F} \cdot d\mathbf{l} + \int_{AB} \mathbf{F} \cdot d\mathbf{l} + \int_{BC} \mathbf{F} \cdot d\mathbf{l} + \int_{CO} \mathbf{F} \cdot d\mathbf{l}$$

- Now

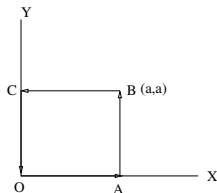
$$\int_{OA} \mathbf{F} \cdot d\mathbf{l} = \int \mathbf{F} \cdot d\mathbf{x}\hat{\mathbf{i}} = \int_0^a (-y)dx = 0, \because y = 0$$

$$\int_{AB} \mathbf{F} \cdot d\mathbf{l} = \int \mathbf{F} \cdot dy\hat{\mathbf{j}} = \int_0^a xdy = a \int_0^a dy = a^2$$

$$\int_{BC} \mathbf{F} \cdot d\mathbf{l} = \int \mathbf{F} \cdot dx\hat{\mathbf{i}} = \int_a^0 (-y)dx = -a \int_a^0 dy = a^2$$

$$\int_{CO} \mathbf{F} \cdot d\mathbf{l} = \int \mathbf{F} \cdot dy\hat{\mathbf{j}} = \int_a^0 xdy = 0, \because x = 0$$

# Stokes theorem, example...



- Thus, LHS of Stokes theorem yields

$$\oint \mathbf{F} \cdot d\mathbf{l} = a^2 + a^2 = 2a^2$$

- Let us calculate the RHS

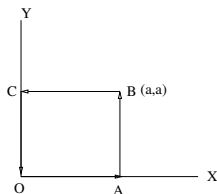
$$\int (\nabla \times \mathbf{F}) \cdot d\mathbf{S}$$

- It is obvious that

$$\nabla \times \mathbf{F} = 2\hat{\mathbf{k}}$$

$$d\mathbf{S} = dx dy \hat{\mathbf{k}}$$

# Stokes theorem verified



- So that

$$\int (\nabla \times \mathbf{F}) \cdot d\mathbf{S} = 2 \int dx \int dy = 2a^2$$

- Thus

$$\text{LHS} = \text{RHS}$$

- Stokes theorem stands verified for this case

# Stokes theorem and Conservative Forces

- For a general vector field  $\mathbf{F}$ , Stokes theorem states

$$\oint \mathbf{F} \cdot d\mathbf{l} = \int_S (\nabla \times \mathbf{F}) \cdot d\mathbf{S}.$$

- If  $\mathbf{F}$  is a conservative force, then we know

$$\oint \mathbf{F} \cdot d\mathbf{l} = 0.$$

- The surface area enclosed by a closed loop, in general, is nonzero
- Therefore, for a conservative force  $\mathbf{F}$ , Stokes theorem implies

$$\nabla \times \mathbf{F} = 0.$$

- Thus, all conservative forces have vanishing curl.

# Curl of Conservative Forces

- We also saw that a conservative force can be expressed as

$$\mathbf{F} = -\nabla V(\mathbf{r}) = -\frac{\partial V}{\partial x}\hat{\mathbf{i}} - \frac{\partial V}{\partial y}\hat{\mathbf{j}} - \frac{\partial V}{\partial z}\hat{\mathbf{k}}$$

- Let us calculate the curl of  $\mathbf{F}$

$$\nabla \times \mathbf{F} = \begin{vmatrix} \hat{\mathbf{i}} & \hat{\mathbf{j}} & \hat{\mathbf{k}} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ -\frac{\partial V}{\partial x} & -\frac{\partial V}{\partial y} & -\frac{\partial V}{\partial z} \end{vmatrix}$$

- We obtain

$$\begin{aligned} \nabla \times \mathbf{F} &= \left( -\frac{\partial^2 V}{\partial y \partial z} + \frac{\partial^2 V}{\partial z \partial y} \right) \hat{\mathbf{i}} + \left( -\frac{\partial^2 V}{\partial z \partial x} + \frac{\partial^2 V}{\partial x \partial z} \right) \hat{\mathbf{j}} \\ &\quad + \left( -\frac{\partial^2 V}{\partial x \partial y} + \frac{\partial^2 V}{\partial y \partial x} \right) \hat{\mathbf{k}} \\ &= 0 \end{aligned}$$

- Right hand side vanishes term by term because

$$\frac{\partial^2 V}{\partial y \partial z} = \frac{\partial^2 V}{\partial z \partial y} \text{ etc.}$$

- The result obtained above: Curl of a conservative force vanishes, is due to the general result: curl of gradient of any scalar function vanishes

$$\nabla \times (\nabla \Phi) = 0,$$

where  $\Phi(\mathbf{r})$  is any scalar function.

## Example: Obtaining potential from the force

- This can be done by integrating the partial differential equation (PDE)

$$-\nabla V = \mathbf{F},$$

- For 3D case, this amounts to integrating three PDEs

$$\frac{\partial V}{\partial x} = -F_x$$

$$\frac{\partial V}{\partial y} = -F_y$$

$$\frac{\partial V}{\partial z} = -F_z$$

- We illustrate the method by a 2D case, where  $\mathbf{F}$  is

$$\mathbf{F} = A(x^2\hat{\mathbf{i}} + y\hat{\mathbf{j}})$$

- First we check whether  $\nabla \times \mathbf{F} = 0$ , or not?
- If  $\nabla \times \mathbf{F} \neq 0$ , then one cannot find a  $V(\mathbf{r})$  which satisfies  $-\nabla V = \mathbf{F}$ .

# Obtaining potential from force



$$\nabla \times \mathbf{F} = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ Ax^2 & Ay & 0 \end{vmatrix} = (0)\hat{i} + (0)\hat{j} + (0)\hat{k} = 0$$

- Thus,  $\mathbf{F}$  is a conservative force, and will satisfy

$$\frac{\partial V}{\partial x} = -Ax^2$$
$$\frac{\partial V}{\partial y} = -Ay$$

- On integrating the  $x$  equation, we have

$$V(x, y) = -\frac{Ax^3}{3} + f(y),$$

where  $f(y)$  is an unknown function of  $y$ .

- On substituting this in  $y$  equation we have

$$\frac{\partial}{\partial y} \left( -\frac{Ax^3}{3} + f(y) \right) = -Ay$$

# Obtaining potential from force



$$\nabla \times \mathbf{F} = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ Ax^2 & Ay & 0 \end{vmatrix} = (0)\hat{i} + (0)\hat{j} + (0)\hat{k} = 0$$

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- We have

$$\frac{\partial f}{\partial y} = \frac{df}{dy} = -Ay$$
$$\implies f(y) = -\frac{Ay^2}{2} + C$$

- Leading to the final result

$$V(x, y) = -\frac{Ax^3}{3} - \frac{Ay^2}{2} + C$$